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**Héroux**

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(54) **DOUBLE MIRROR STRUCTURE FOR WAVELENGTH DIVISION MULTIPLEXING WITH POLYMER WAVEGUIDES**

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See application file for complete search history.

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**G02B 6/132** (2006.01)

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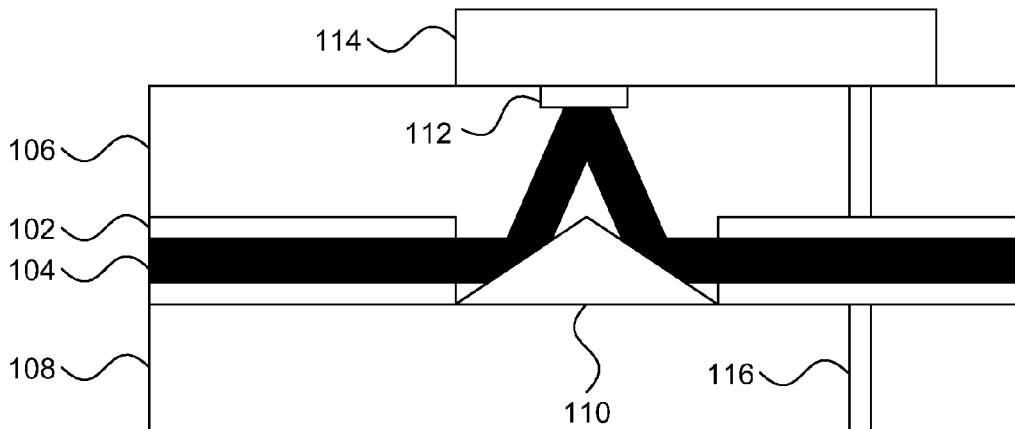
(52) **U.S. Cl.**  
CPC ..... **G02B 6/12007** (2013.01); **G02B 6/132** (2013.01); **G02B 6/4214** (2013.01); **G02B 6/4215** (2013.01); **G02B 2006/12109** (2013.01);  
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(57) **ABSTRACT**

Methods for wavelength filtering and structures for accomplishing the same. Wavelength filtering includes forming grooves in a waveguide to define angled surfaces in a path of the waveguide; forming a reflective layer on the angled surfaces; depositing cladding material on top of the waveguide and on the angled surfaces; forming a filter layer on an active region of an opto-electronic device, which transmits a single wavelength and reflects other wavelengths used; depositing the opto-electrical device on the cladding layer such that the filter layer is aligned with a point of incidence of a light beam reflected from the reflective layer; and electrically bonding the opto-electronic device to vias in the waveguide structure.

(58) **Field of Classification Search**  
CPC ..... G02B 6/4215; G02B 6/4214; G02B 6/43; G02B 27/143; G02B 6/3512; H01L 33/60

**19 Claims, 8 Drawing Sheets**



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(2015.01)

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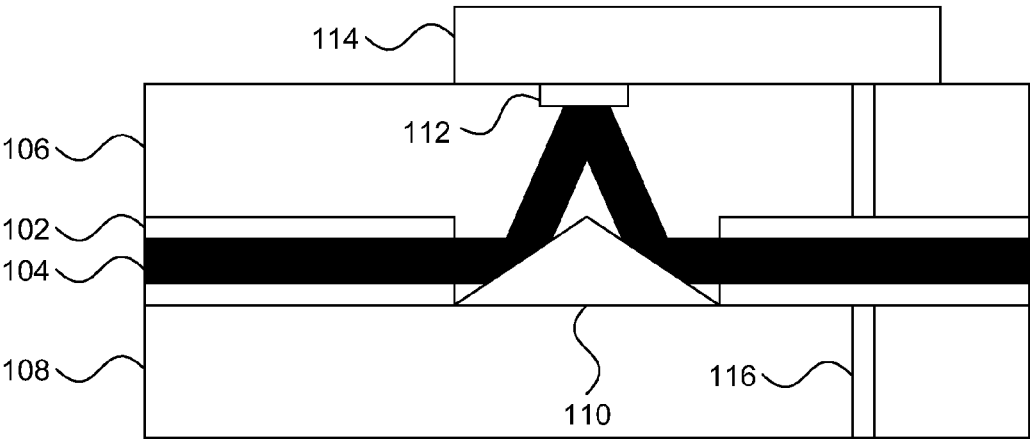


FIG. 1

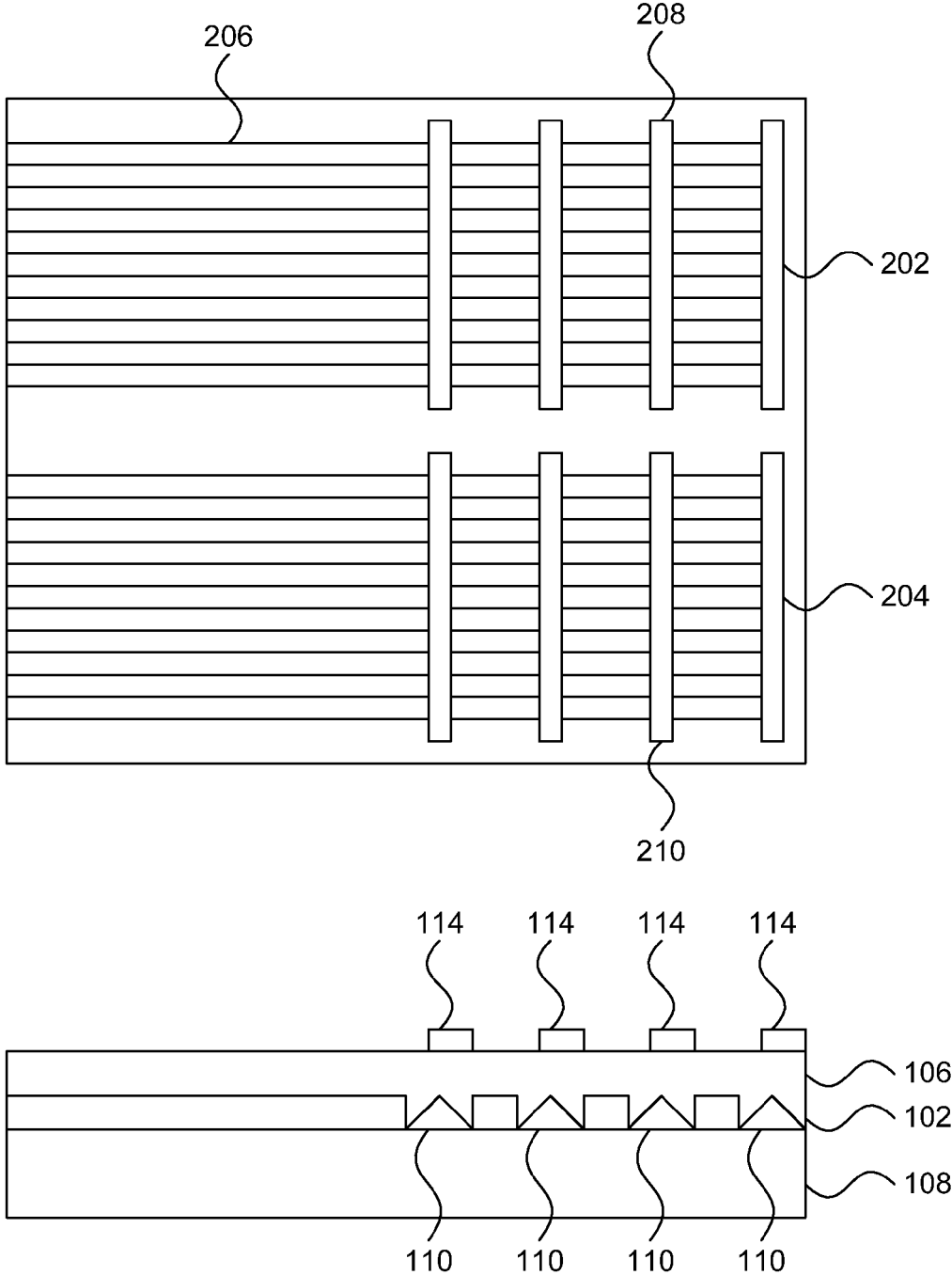


FIG. 2

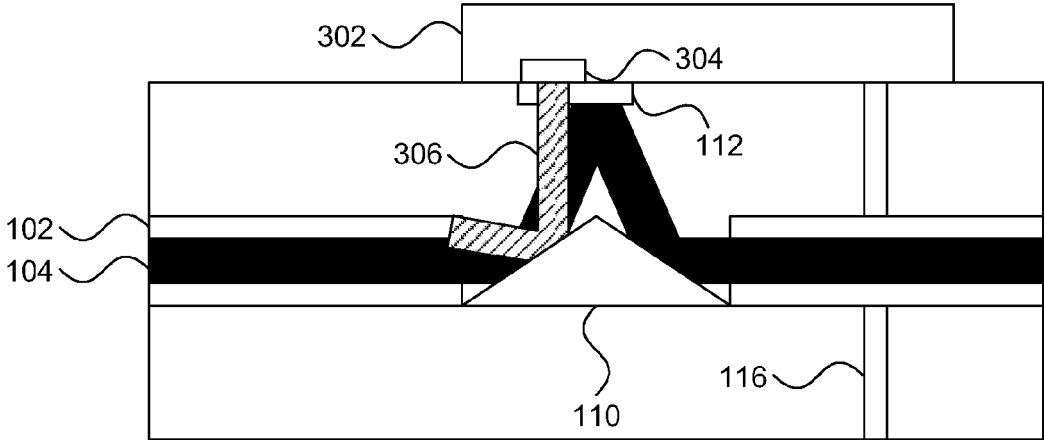


FIG. 3

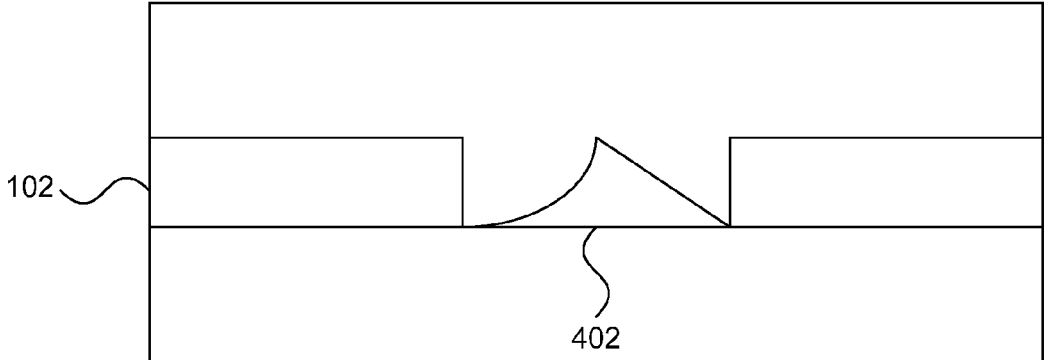


FIG. 4

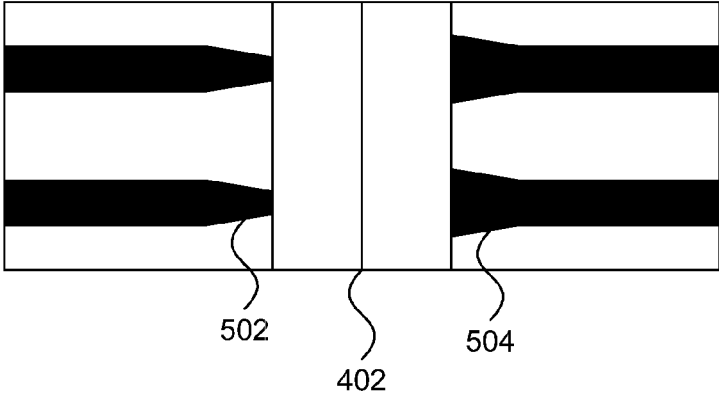


FIG. 5

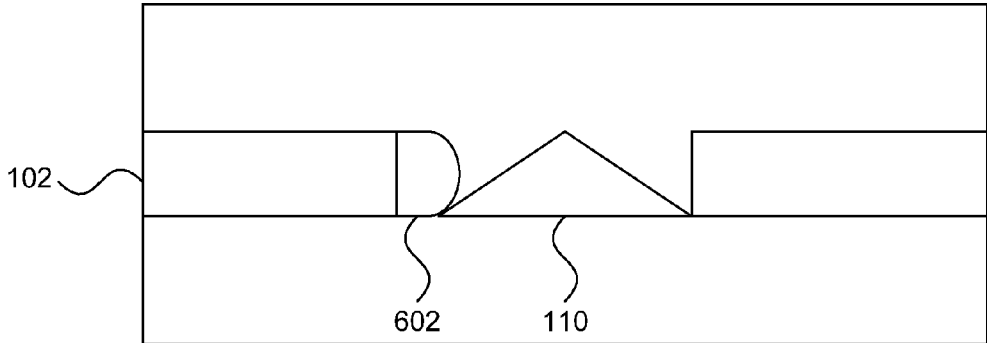


FIG. 6

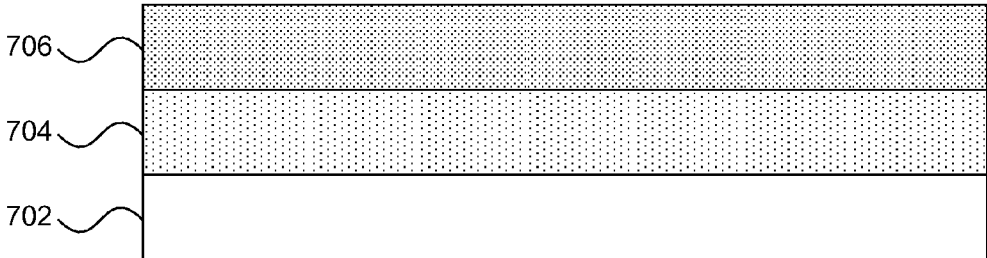


FIG. 7

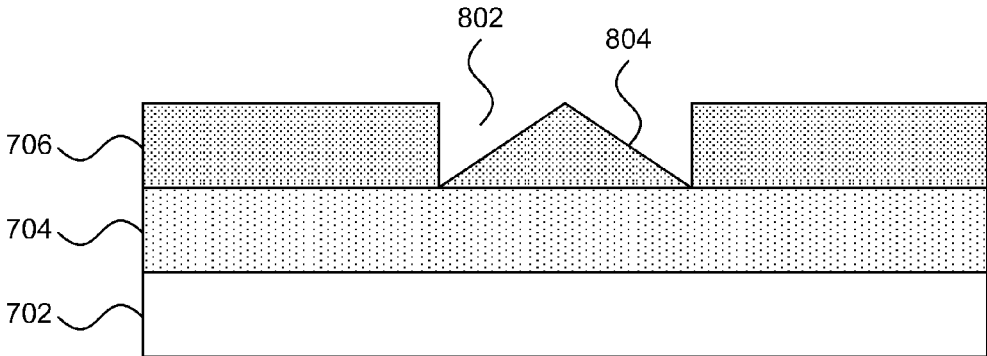


FIG. 8

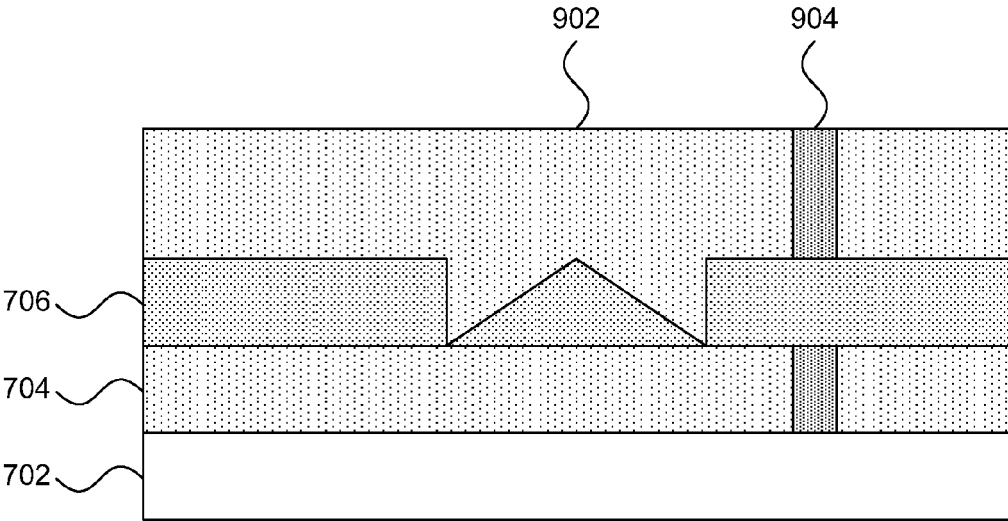


FIG. 9

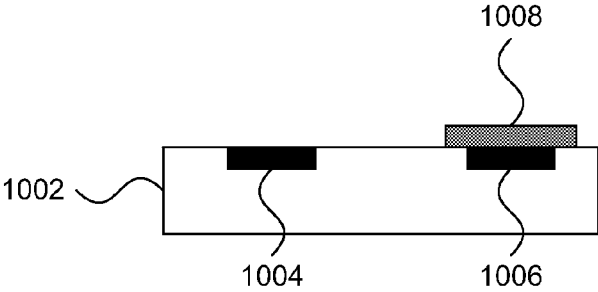


FIG. 10

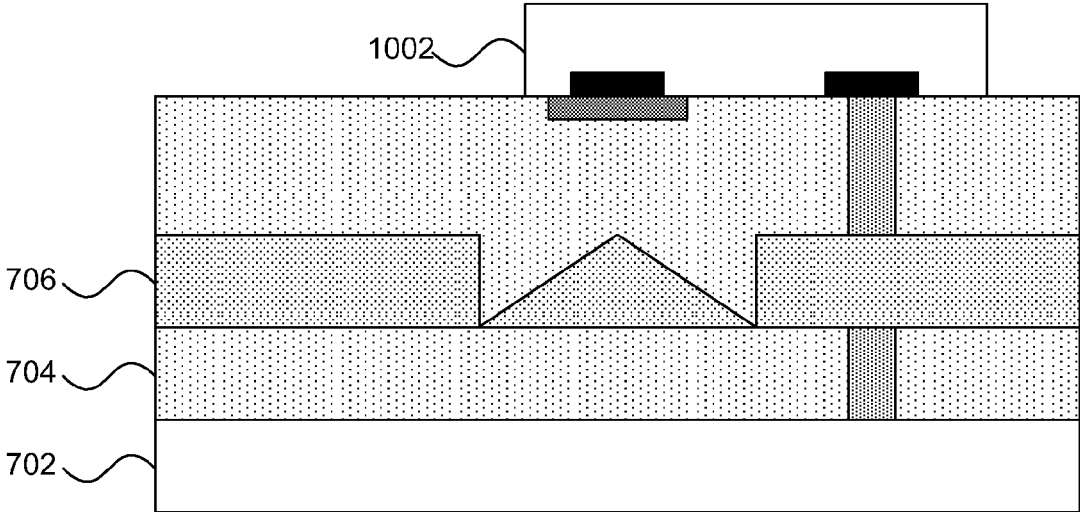


FIG. 11



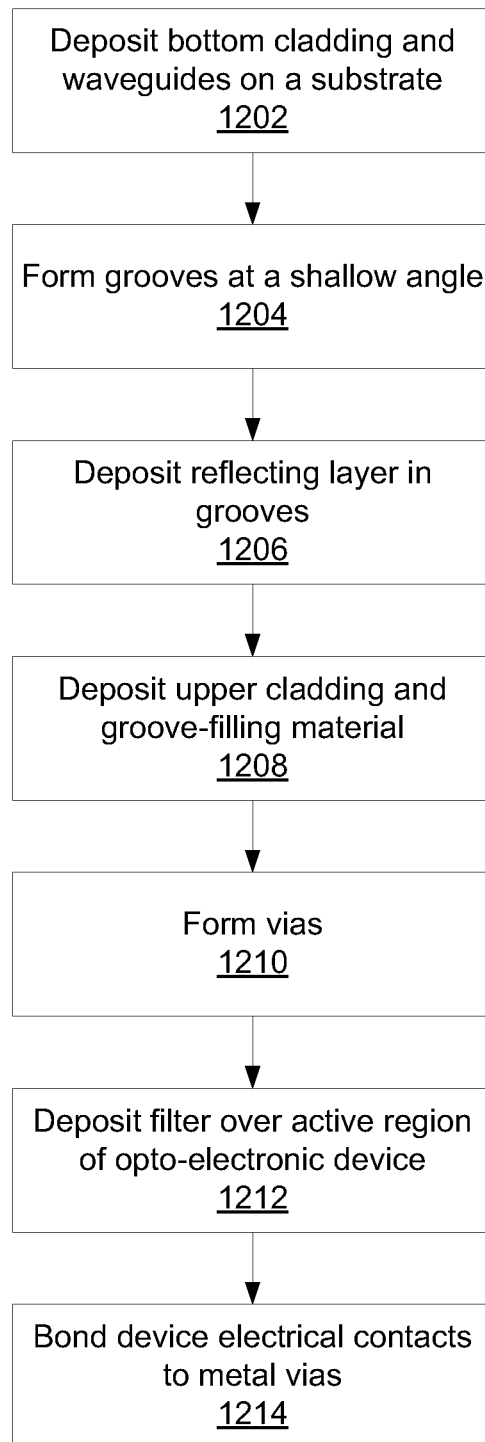


FIG. 12

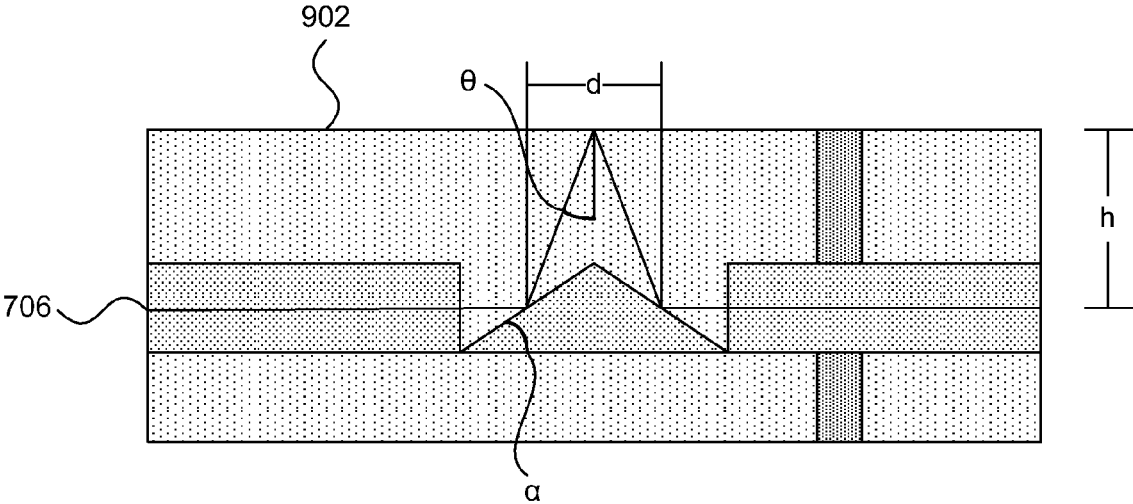


FIG. 13

## DOUBLE MIRROR STRUCTURE FOR WAVELENGTH DIVISION MULTIPLEXING WITH POLYMER WAVEGUIDES

### RELATED APPLICATION INFORMATION

This application is a Continuation application of co-pending U.S. patent application Ser. No. 14/067,535, filed on Oct. 30, 2013, which is incorporated herein by reference in its entirety.

### BACKGROUND

#### 1. Technical Field

The present invention relates to fiber optics systems and, more particularly, to wavelength division multiplexing with polymer waveguides.

#### 2. Description of the Related Art

Optical data transfer is increasingly used in high-performance computing, where short-range optical communication provides a fast and low power alternative to electrical communication. However, despite these developments, new multi-core processing architectures demand higher bandwidth and density. The number of channels needed to transfer information is increasing rapidly. In the most advanced systems, more than 60,000 individual fibers are used, so that practical physical limits are being rapidly reached.

Efforts have been made to use a single fiber to carry multiple data signals at different wavelengths. This increases the total bandwidth of a system without a corresponding increase in the number of physical channels, but existing wavelength division multiplexing solutions are difficult to implement on optical printed circuit board technology. In one notable example, a dielectric mirror is formed in a waveguide at a forty-five degree angle to the direction of transmission. The mirror is made to be selectively reflective, such that one wavelength is reflected out of the waveguide path while the other wavelengths are passed through.

However, it is difficult to form such a reflector on a polymer waveguide, it is difficult to form structures on a forty-five degree angle due to shadow effects, and the reflector itself must be relatively thick due to a large polarization dependency that results from the forty-five degree angle of incidence.

### SUMMARY

A wavelength filtering structure includes a first reflective surface, positioned at an end of a first waveguide section, that reflects a beam comprising a plurality of wavelengths; a filter in the path of the reflected beam that allows a selected wavelength from the reflected beam to pass and that reflects all other wavelengths in a selected beam; and a second reflective surface, positioned adjacent to the first reflective surface and at an end of a second waveguide section, that reflects the selected beam into a core of the second waveguide section.

A wavelength division multiplexer/demultiplexer includes a plurality of filtering structures formed next to each other on a board, each transmitting a different wavelength from a beam comprising a plurality of wavelengths. Each filtering structure includes a first reflective surface, positioned at an end of a first waveguide section, that reflects the beam comprising a plurality of wavelengths, formed at an angle less than 45 degrees relative to a beam path and having a curve to compensate for beam divergence; a filter in the path of the reflected beam that allows the selected wavelength from the reflected beam to be transmitted and that reflects all other

wavelengths in a selected beam; and a second reflective surface, positioned adjacent to the first reflective surface and at an end of a second waveguide section, that reflects the selected beam to the end of the second waveguide section, formed at an angle less than 45 degrees relative to the beam path.

A method for forming a wavelength filtering structure includes forming grooves in a waveguide to define angled surfaces in a path of the waveguide; forming a reflective layer on the angled surfaces; depositing cladding material on top of the waveguide and on the angled surfaces; forming a filter layer on an active region of an opto-electronic device, which transmits a single wavelength and reflects other wavelengths used; depositing the opto-electrical device on the cladding layer such that the filter layer is aligned with a point of incidence of a light beam reflected from the reflective layer; and electrically bonding the opto-electronic device to vias in the waveguide structure.

These and other features and advantages will become apparent from the following detailed description of illustrative embodiments thereof, which is to be read in connection with the accompanying drawings.

### BRIEF DESCRIPTION OF DRAWINGS

The disclosure will provide details in the following description of preferred embodiments with reference to the following figures wherein:

FIG. 1 is a cross-sectional view of a section of a wavelength demultiplexer structure in accordance with the present principles;

FIG. 2 is a top-down and side view of a wavelength division multiplexing transceiver in accordance with the present principles;

FIG. 3 is a cross-sectional view of a section of a wavelength multiplexer in accordance with the present principles;

FIG. 4 is a cross-sectional view of a curved mirror structure in accordance with the present principles;

FIG. 5 is a top-down view of waveguides in accordance with the present principles;

FIG. 6 is a cross-sectional view of a waveguide focusing element in accordance with the present principles;

FIG. 7 is a cross-sectional view of a step in forming a wavelength filter structure in accordance with the present principles;

FIG. 8 is a cross-sectional view of a step in forming a wavelength filter structure in accordance with the present principles;

FIG. 9 is a cross-sectional view of a step in forming a wavelength filter structure in accordance with the present principles;

FIG. 10 is a cross-sectional view of a step in forming a wavelength filter structure in accordance with the present principles;

FIG. 11 is a cross-sectional view of a step in forming a wavelength filter structure in accordance with the present principles;

FIG. 12 is a block/flow diagram of a method of forming a wavelength filter structure in accordance with the present principles; and

FIG. 13 is a cross-sectional view of geometric relationships in a wavelength filter structure in accordance with the present principles.

### DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

Embodiments of the present invention provide wavelength division multiplexing (WDM) in a polymer waveguide struc-

ture having an array of cores with a high density. The present embodiments use a double mirror structure with a dielectric filter deposited on an opto-electronic device array or on the top cladding to form wavelength filters. Although it is specifically contemplated that polymer waveguides be used in the present embodiments, it should be recognized that the present principles may be readily extended to other types of waveguide. Polymer waveguides and micromirrors guide the light from laser arrays with a high density, for example a 125 um core pitch. The signals from a board can be sent directly to another board via polymer waveguides for short range integrated data transfer, or can be coupled to a fiber ribbon for longer range data transfer.

Referring now to the drawings in which like numerals represent the same or similar elements and initially to FIG. 1, a WDM mirror structure is shown. A waveguide core layer **102** is formed with an upper cladding **106** and a lower cladding **108**. The waveguide carries a beam **104** that includes several different wavelengths. In the present examples the beam **104** is described with respect to four wavelengths,  $\lambda_1$ ,  $\lambda_2$ ,  $\lambda_3$ , and  $\lambda_4$ , but it is contemplated that any number of mutually non-interfering wavelengths may be used.

In a receiver configuration, the beam **104** is reflected by a two-sided mirror structure **110** at an angle of incidence larger than forty-five degrees. The mirror structure **110** may be formed with a surface of gold or some other appropriate reflective material that has little loss at the wavelengths of the beam **104**. The beam **104** then exits the plane of the waveguide **102** through the upper cladding **106** to reach a dielectric filter **112**. The dielectric filter is transparent to only one of the wavelengths, e.g.,  $\lambda_1$ , which reaches a detector device **114**. The remaining wavelengths are reflected from the dielectric filter **112**, reflect off of mirror **110**, and reenter the waveguide **102**. It is anticipated that the detector **114** may send an electrical signal corresponding to the received light through electrical via **116**, but it should be understood that additional processing may occur as well and other electrical contact configurations such as a planar line on top of the clad layer **106** are also possible.

It is to be understood that the present invention will be described in terms of a given illustrative architecture having a laminar substrate and waveguide-integrated organic carrier; however, other architectures, structures, substrate materials and process features and steps may be varied within the scope of the present invention.

It will also be understood that when an element such as a layer, region or substrate is referred to as being "on" or "over" another element, it can be directly on the other element or intervening elements may also be present. In contrast, when an element is referred to as being "directly on" or "directly over" another element, there are no intervening elements present. It will also be understood that when an element is referred to as being "connected" or "coupled" to another element, it can be directly connected or coupled to the other element or intervening elements may be present. In contrast, when an element is referred to as being "directly connected" or "directly coupled" to another element, there are no intervening elements present.

A design for a polymer waveguide may be created in a graphical computer programming language, and stored in a computer storage medium (such as a disk, tape, physical hard drive, or virtual hard drive such as in a storage access network). If the designer does not fabricate waveguides or the photolithographic masks used to fabricate waveguides, the designer may transmit the resulting design by physical means (e.g., by providing a copy of the storage medium storing the design) or electronically (e.g., through the Internet) to such

entities, directly or indirectly. The stored design is then converted into the appropriate format (e.g., GDSII) for the fabrication of photolithographic masks, which typically include multiple copies of the design in question that are to be formed on a polymer substrate. The photolithographic masks are utilized to define areas of the substrate (and/or the layers thereon) to be etched or otherwise processed.

Reference in the specification to "one embodiment" or "an embodiment" of the present principles, as well as other variations thereof, means that a particular feature, structure, characteristic, and so forth described in connection with the embodiment is included in at least one embodiment of the present principles. Thus, the appearances of the phrase "in one embodiment" or "in an embodiment", as well as any other variations, appearing in various places throughout the specification are not necessarily all referring to the same embodiment.

It is to be appreciated that the use of any of the following "and/or", "and/or", and "at least one of", for example, in the cases of "A/B", "A and/or B" and "at least one of A and B", is intended to encompass the selection of the first listed option (A) only, or the selection of the second listed option (B) only, or the selection of both options (A and B). As a further example, in the cases of "A, B, and/or C" and "at least one of A, B, and C", such phrasing is intended to encompass the selection of the first listed option (A) only, or the selection of the second listed option (B) only, or the selection of the third listed option (C) only, or the selection of the first and the second listed options (A and B) only, or the selection of the first and third listed options (A and C) only, or the selection of the second and third listed options (B and C) only, or the selection of all three options (A and B and C). This may be extended, as readily apparent by one of ordinary skill in this and related arts, for as many items listed.

Referring now to FIG. 2, a WDM transceiver is shown. A WDM demultiplexer is made out of four photodetector arrays **202** that receive light from the waveguide array **206**, each core initially carrying four different wavelengths. The wavelength-specific filters **208** each transmit only one of the wavelengths and reflect the others, such that the fourth and final filter **208** transmits the final remaining wavelength. After transmission through the filters, light from each core reaches the active regions of a detector. In a preferred embodiment, the detectors are semiconductor photodiode arrays electrically linked to a trans-impedance limiting amplifier integrated circuit.

A WDM multiplexer **204** has the reverse light path from the WDM demultiplexer, with the four wavelength-specific filters **210** on top of a second waveguide array **206**. Each of the filters **210** transmits light at one of the four wavelengths and reflects light at the other wavelengths. It should be noted that the number of wavelengths could be smaller or greater than four for the multiplexer and the demultiplexer.

In one exemplary embodiment, the demultiplexer **202** may receive light signals at the wavelengths 850 nm, 980 nm, 1020 nm, and 1060 nm. At the first wavelength-specific filter **208**, the 850 nm wavelength may be transmitted, leaving the 980 nm, 1020 nm, and 1060 nm light signals to be reflected back inside the waveguides **206**. Similarly, the second wavelength-specific filter **208** transmits the 980 nm light signal and reflects the 1020 nm and 1060 nm light signals. The third filter **208** transmits 1020 nm, and the final light signal at 1060 nm is transmitted to the photodiode **204**. Conversely, for the multiplexer, the wavelength-specific filters **210** combine the light signals at the four wavelengths emitted from the laser arrays **204**, which emit light at 850, 980, 1020 and 1060 nm respectively.

A cross-sectional side view is also shown that illustrates each of the filters **208** as including a detector device **114** and a mirror structure **110**. The actual filter **112** is very small relative to the size of the device **114** and the mirror structure **110** and is not shown here for the sake of simplicity.

Referring now to FIG. **3**, a wavelength-specific transmitter is shown. An electrical signal reaches the emitter device **302** from an electrical via **116** or other electrical configuration so that the emitter **304** emits light at a specified wavelength. The emitter **304** is specifically contemplated as being a vertical cavity surface emitting laser (VCSEL) array, though it is contemplated that other emitters might also be employed. The filter **112** is transparent to the emission wavelength of the emitter **304** directly above it, but reflects light coming from the mirror **110** and emitted by the other emitters **304**. The combined light signal re-enters the waveguide core **104**. As VCSELs emit light perpendicular to their surface, a slight coupling loss may occur as the light beam enters the waveguide core after reflection from the mirror **110**. However, this loss is typically small and the VCSEL active area has a diameter smaller than the beam, typically in the range of about  $3\mu$  to about  $8\mu\text{m}$ . As an alternative embodiment, an asymmetric lens may be fabricated on the emitter **304** to make the emitted light beam **306** parallel to the other beam **104**.

One potential difficulty with the double-mirror structures described above can be found in the fact that the beams **104** will have a small divergence angle as they exit the waveguide **102**, resulting in some coupling loss. The beams **104** may be propagated for a distance of, e.g.,  $200\mu\text{m}$  before reentering the waveguide **102**. The mirror structure **110** and the ends of the waveguides **102** may be formed to accommodate and correct for these losses.

Referring now to FIG. **4** a modified double mirror structure is shown. In contrast to the mirror-structure **110** shown above, which has flat sides, the modified mirror structure **402** has at least one curved side. The curve may, for example, be along a single axis or may be a paraboloid shape. Only one face of the modified mirror structure **402** needs to be curved, and the curved face should preferably be the one on which light coming out of the waveguide is first reflected.

A single-axis curve, as shown, is easier to fabricate but can only correct for divergence in one direction, while a parabolic or elliptical mirror will be able to collimate light in both directions but will be more difficult to fabricate. To account for the second axis of divergence when using a single-axis curved mirror **402**, the waveguides **102** may be tapered, both before and after the beam is reflected on the mirror **402**.

Referring now to FIG. **5**, tapered waveguides to compensate for planar beam divergence are shown. The core of the waveguide **502** from which light is coming becomes smaller closer to the curved mirror structure **402**, decreasing the beam size before it is reflected. After the beam is reflected by the second surface of the mirror structure **402**, it re-enters the waveguide **504**. The core of the waveguide **504** is widened so that a higher portion of the diverging light beam can be guided into the core. The core size is gradually decreased to its initial standard value. The combination of smaller core size on one side of the waveguide and larger size on the other helps to minimize loss due to beam divergence in the plane of the waveguides.

Referring now to FIG. **6**, an alternative embodiment is shown that uses a focusing element **602** that is separate from the mirror structure **110**. In this embodiment a portion of the waveguide **102** near the mirror structure **110** is removed to make space for a lens array **602**. This lens array **602** may be a single unit that is inserted across multiple waveguides **102** and can be made, for example, from glass or polymer.

Referring now to FIG. **7**, a step in creating a WDM mirror structure is shown. A lower cladding **704** and a polymer waveguide material **706** are formed on a substrate **702**. The waveguide material **706** is deposited in a layer and a core pattern is formed by using a lithography technique or other optical method to slightly alter the refractive index of the material. The substrate may be, for example, an FR4-grade board formed from glass-reinforced epoxy laminate sheets, but it is contemplated that any appropriate material may be used instead.

Referring now to FIG. **8**, a step in creating a WDM mirror structure is shown. Two grooves **802** are formed in the waveguide material **706** for each wavelength expected in beam **104**. The grooves **802** are formed such that a shallow-angled surface is formed, having an angle of less than forty-five degrees. A reflecting layer **804** is deposited on the surfaces of the remaining waveguide material **706** forming the bottom of the grooves **802**. The reflector **804** may be formed from, e.g., gold or any other suitable material that will reflect all operation wavelengths. To form the reflector **804**, a mask may be positioned over the waveguide material **706** to expose only the grooves **802** and the reflective material may be deposited using one of, e.g., evaporation, sputtering, atomic layer deposition, chemical vapor deposition, etc.

Referring now to FIG. **9**, an additional cladding layer **902** is deposited on top of the core layers and in the grooves. Vias **904** are created that go through the cladding **704/902**. The vias **904** are formed by drilling or etching holes in the cladding **704/902** using a method such as, e.g., laser drilling. A conductor is then deposited in the holes, creating a conductive link between the top of the cladding and the board underneath the bottom cladding layer.

Referring now to FIG. **10**, an opto-electronic device **1002** is formed separately. As described above, the device **1002** may be a detector or a laser array (e.g., a semiconductor photodiode array and a VCSEL array) for a specific wavelength. The device **1002** has metal pads **1004** and an active region **1006** to emit or absorb light. A filter **1008** is deposited on the active region **1006** and is transparent to one of the wavelengths expected in beam **104**. The filter **1008** therefore allows the selected wavelength to be transmitted to or from the device active region **1006** and reflects the other wavelengths. The filter **1008** may be, for example, a distributed Bragg reflector or some other photonic crystal structure formed using, e.g., a quarter wave stack of two dielectric materials such as  $\text{SiO}_2/\text{TiO}_2$  deposited by evaporation. Semiconductor materials or other types of filters, such as colored glass, can also be used.

Referring now to FIG. **11**, the opto-electronic device **1002** is flip-bonded to the upper cladding **902** and electrical contact using, for example, C4 bonding. The electrical device **1002** is positioned such that the metal pads **1004** align with the via **904** and the filter **1008** is over the reflector **804**. The specific alignment of the filter **1008** and the receiver/transmitter **1006** with respect to the reflector **804** will vary depending on whether the opto-electronic device **1002** is a detector, in which case the receiver **1006** will be aligned with the reflected beam, or as a transmitter, in which case the transmitter may be slightly off-center to minimize the coupling loss with a waveguide core **706**. It should be noted that the present figures are not drawn to scale—the thickness of the filter **1008** may be about  $2\text{-}5\mu\text{m}$  thick, which is negligible compared to the process variation of the cladding surface.

Referring now to FIG. **12**, a block/flow diagram of the fabrication of a double mirror WDM structure is shown. In block **1202**, a lower cladding **704** is deposited on a board **702**. The core layer **706** is then deposited, and the cores are formed

using lithography or other technique. In block **1204**, grooves **802** at a shallow angle are formed in the waveguide material **706** to produce a double-sided structure. In block **1206**, a layer **804** is deposited in the grooves by, e.g., evaporation or other technique that is reflective at all the operation wavelengths. In block **1208**, an upper cladding **902** is deposited on top of the reflector **708** and core layer **706**. In block **1210**, vias **904** are formed by drilling or etching a hole in the waveguide layers **902/706/704** and filling the hole with a conductive material.

In block **1212**, a filter **1108** is deposited on the active region of a laser or detector array **1006**. The filter **1008** is transparent to one specific wavelength out of the operating wavelengths, such that any other wavelength is reflected. In block **1214**, the emitter/receiver **1002** is flip-chip bonded to the upper cladding **902** such that the filter **1008** is positioned over the reflector **804** and the device **1002** is electrically connected to the vias **904**.

Referring now to FIG. **13**, the upper cladding layer **902** is shown with dimensional considerations. The thickness of the upper cladding layer **902**, as well as the unguided light path length depends on the dimensions of the reflector **804**. In particular, the height  $h$  of the cladding layer **902** can be expressed as  $h=d/2 \tan(\theta)$ , where  $d$  is the horizontal distance between the beam incident on the reflector **804** and the beam reflected a second time from the reflector **804**, measured from the middle of the respective beams and  $\theta$  is the angle of incidence of the reflected beam at the top of the cladding layer **902**.  $\theta$  is determined by the angle of the reflector **804** as  $\theta=90^\circ-2\alpha$ , where  $\alpha$  is the angle between the surface of the reflector **804** and the plane of the waveguide core. A minimum value for  $d$ , and hence for  $h$ , may be determined as  $d_{min}=w/\tan(\alpha)$ , where  $w$  is the beam width and is related to the size of the waveguide core size.

Having described preferred embodiments of a double-mirror structure for WDM with polymer waveguides and methods of forming the same (which are intended to be illustrative and not limiting), it is noted that modifications and variations can be made by persons skilled in the art in light of the above teachings. It is therefore to be understood that changes may be made in the particular embodiments disclosed which are within the scope of the invention as outlined by the appended claims. Having thus described aspects of the invention, with the details and particularity required by the patent laws, what is claimed and desired protected by Letters Patent is set forth in the appended claims.

What is claimed is:

1. A wavelength filtering structure, comprising:
  - a first reflective surface, positioned at an end of a first waveguide section, that reflects a beam comprising a plurality of wavelengths;
  - a filter in the path of the reflected beam that allows a selected wavelength from the reflected beam to pass and that reflects all other wavelengths in a selected beam;
  - a second reflective surface, positioned adjacent to the first reflective surface and at an end of a second waveguide section, that reflects the selected beam into a core of the second waveguide section; and
  - an emitter configured to emit the selected wavelength through the filter, wherein the emitter is aligned with the filter.
2. The wavelength filtering structure of claim **1**, wherein the first and second reflective surfaces are formed at an angle relative to the beam path.
3. The wavelength filtering structure of claim **2**, wherein the first and second reflective surfaces are formed at an angle less than 45 degrees relative to the beam path.

4. The wavelength filtering structure of claim **1**, further comprising a photodetector configured to receive the selected wavelength that passes through the filter.

5. The wavelength filtering structure of claim **1**, wherein the emitter comprises a lens configured to orient the emitted light in a direction parallel to the existing beam.

6. The wavelength filtering structure of claim **1**, wherein the emitter is set at a non-zero lateral distance from a point of incidence on the filter where the reflected beam hits.

7. The wavelength filtering structure of claim **6**, wherein the emitted wavelength reflects from the second reflective surface to enter the second waveguide section.

8. The wavelength filtering structure of claim **1**, further comprising a focusing element at an end of the first waveguide section configured to compensate for beam divergence.

9. A wavelength division multiplexer/demultiplexer, comprising:

a plurality of filtering structures formed next to each other on a board, each transmitting a different wavelength from a beam comprising a plurality of wavelengths, each filtering structure including:

a first reflective surface, positioned at an end of a first waveguide section, that reflects the beam comprising a plurality of wavelengths, formed at an angle less than 45 degrees relative to a beam path and having a curve to compensate for beam divergence;

a filter in the path of the reflected beam that allows the selected wavelength from the reflected beam to be transmitted and that reflects all other wavelengths in a selected beam;

a second reflective surface, positioned adjacent to the first reflective surface and at an end of a second waveguide section, that reflects the selected beam to the end of the second waveguide section, formed at an angle less than 45 degrees relative to the beam path; and

an emitter configured to emit the selected wavelength through the filter, wherein the emitter is aligned with the filter.

10. A method for forming a wavelength filtering structure, comprising:

forming grooves in a waveguide to define angled surfaces in a path of the waveguide;

forming a reflective layer on the angled surfaces; depositing cladding material on top of the waveguide and on the angled surfaces;

forming a filter layer on an active region of an opto-electronic device, which transmits a single wavelength and reflects other wavelengths used;

depositing the opto-electronic device on the cladding layer such that the filter layer is aligned with a point of incidence of a light beam reflected from the reflective layer, and such that the filter layer is aligned with an emitter configured to emit the single wavelength through the filter layer; and

electrically bonding the opto-electronic device to vias in the waveguide structure.

11. The method of claim **10**, wherein forming grooves comprises forming the angled surfaces at an angle less than 45 degrees relative to a waveguide axis.

12. The method of claim **10**, wherein the opto-electronic device comprises a photodetector configured to receive the selected wavelength that passes through the filter and wherein said step of bonding comprises bonding a surface of the

electrical device having said photodetector to the cladding layer such that the photodetector is aligned with a point of incidence of a beam.

13. The method of claim 10, wherein said step of bonding comprises bonding a surface of the electrical device having said emitter to the cladding layer such that the emitter is set to a non-zero lateral distance from a point of incidence of a beam.

14. The wavelength filtering structure of claim 1, wherein the first reflective surface has a curve along a single axis to compensate for beam divergence in a single dimension.

15. The wavelength filtering structure of claim 1, wherein the first waveguide section is tapered relative to a carrying width of the first waveguide section, and wherein the second waveguide section is widened relative to a carrying width of the second waveguide section.

16. The wavelength division multiplexer/demultiplexer of claim 9, wherein the first reflective surface has a curve along a single axis to compensate for beam divergence.

17. The wavelength division multiplexer/demultiplexer of claim 9, wherein the first waveguide section is tapered relative to a carrying width of the first waveguide section, and wherein the second waveguide section is widened relative to a carrying width of the second waveguide section.

18. The method of claim 10, further comprising forming a waveguide having a first section that tapers and a second section that is widened relative to a carrying width of the respective waveguide sections.

19. The method of claim 10, wherein one of the grooves is formed with a curve along a single axis of one of the angled surfaces to compensate for beam divergence.

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